

FES 2007 Stormwater Workshop

Stormwater Permitting Course-2007

The Omni Orlando Resort at ChampionsGate

Devo Seereeram, PhD, PE Devo Engineering



- 1. Today's presentation will tell a story which, since the mid 1990's, has been repeated many times by the author. However, it only gets serious attention from drainage engineers and regulators when we have significant cumulative rainfall surpluses or deficits
- 2. The range and magnitude of water level fluctuation in closed (a.k.a. land-locked) lakes, ponds (both wet & dry), and wetlands are linked closely to surpluses and deficits in cumulative rainfall over relatively long periods of time. A "long" period, in this sense, refers to a duration of 1 month to say 42 months. The "critical duration" for a land-locked basin depends on the characteristics of the contributing watershed (time lag before ground water enters) and the geology and geometry of the "pond".

- 3. Current regulations (FDOT & SRWMD) model storm events up to 10 days in duration which don't reflect the true "critical duration" for these closed basins. After all, is 24.11 inches of rainfall in one month for critical than 10.6 inches of rain in 1 day? Is 220 inches of rainfall in 36 months (3 years) more critical than the design 100 yr storm event?
- 4. First data slide will show a plot of recent ground water level trends to get a feel for the actual range of water table fluctuation measured on a Clermont sand ridge over the past 13 years (1994 to the present). This period was somewhat wild and covers 2 major droughts (2001, 2007) and several periods of high rainfall including Tropical Storm Gordon, 1994-1996, El Nino Rains in early 1998, troika of hurricanes in 2004, and record monthly rainfall total in June 2005.

- 5. Analyze cumulative rainfall patterns over the last 100 years at 2 rainfall stations in Central Florida (Orlando International Airport and Clermont) and mark their peaks and valleys for various "critical durations" ranging from 1 month to 48 months. Compare the 1 month totals to the FDOT 100 yr/10 day storm which is the highest rainfall storm currently regulated.
- 6. A quick comparison is done for a site in Seminole County (Lake Sylvan) to compare to cumulative rainfall patterns at OIA. The purpose of this is to show trend similarity between rainfall stations 25 miles apart.
- 7. A summary of the regulatory criteria for each agency will be presented. How applicable are these criteria for providing true regulation of peak stages and duration in these systems?

- 8. Examples of recent flooding in land-locked lakes. Show a rainfall trending analysis and high water stage correlation for 2 lakes which flooded in the Lake Wales area of Polk County (SWFWMD).
- 9. Long-term continuous simulation modeling: discuss the conceptual models, technology and software
- 10. Show some real-world applications of continuous simulation modeling
- 11. Geotechnical Pitfalls in stormwater design will discuss some of these bonus slides if time permits



Review of Long Term Cumulative Rainfall Patterns & Recent Trends in Central Florida



Applicability of Current Regulatory Criteria for Ensuring Flood Protection in Land-Locked Drainage Systems



Long-term and short-term continuous simulation modeling of stormwater management systems.



Some Screen Shots of PONDS 3.2 Software Continuous Simulation Hydrograph Generator



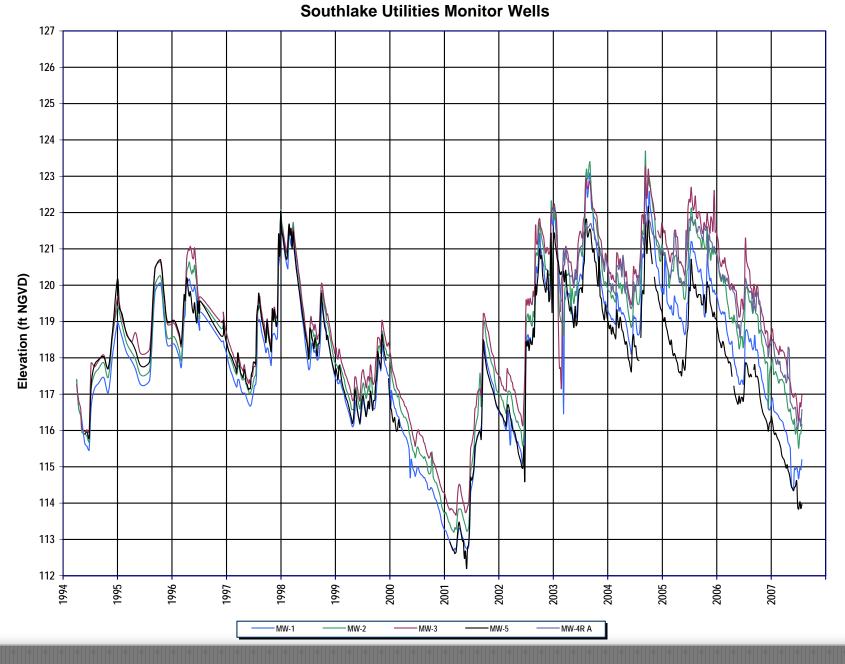
Some lessons in stormwater management design learned from post-mortem investigations

Part 1

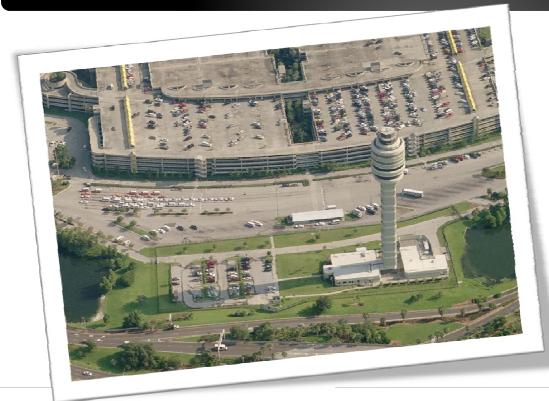
Review of Long Term Cumulative Rainfall Patterns & Recent Trends in Central Florida

Groundwater Levels at Southlake Utilities on Lake Wales Ridge

What has been the measured groundwater level fluctuation on the Central Florida ridge for the past 13 years? Let us look at the trends on a sandhill site which has been continuously monitored since 1994.

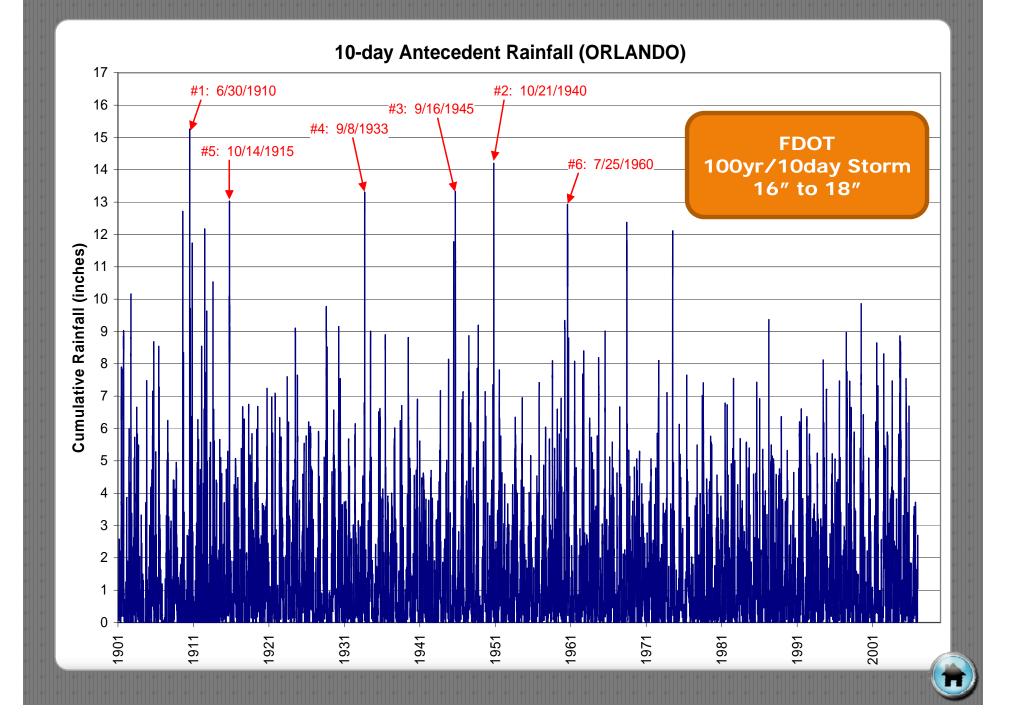


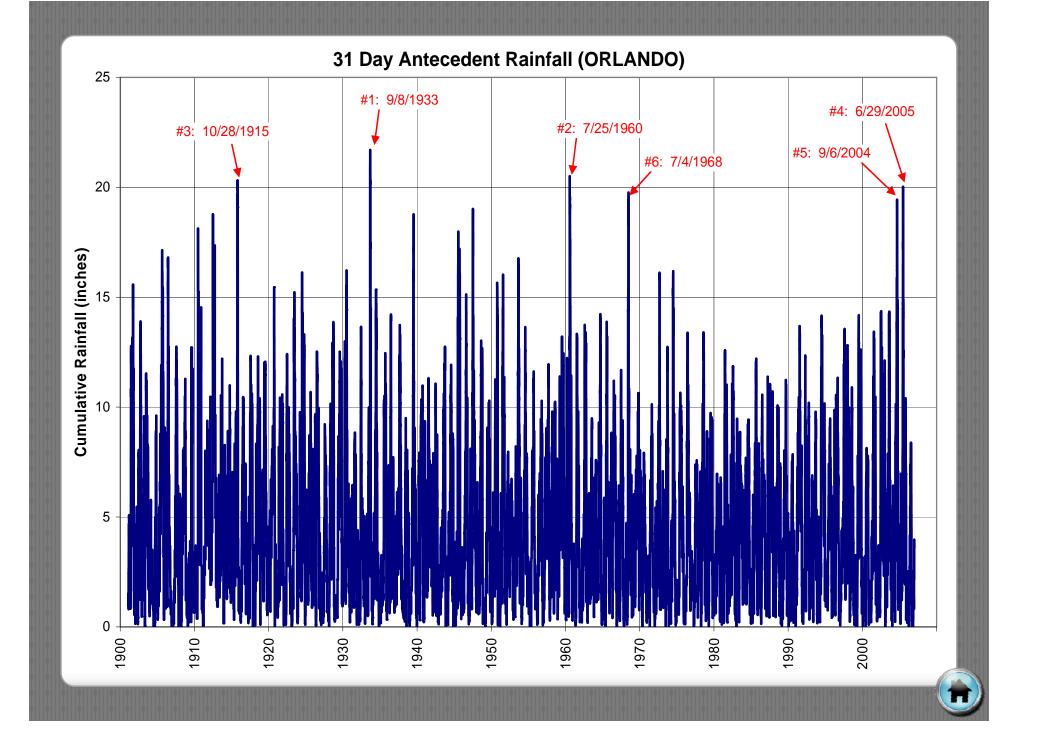
106 Years of Rainfall Data at OIA



Yearly Cumulative Rainfall (Orlando)





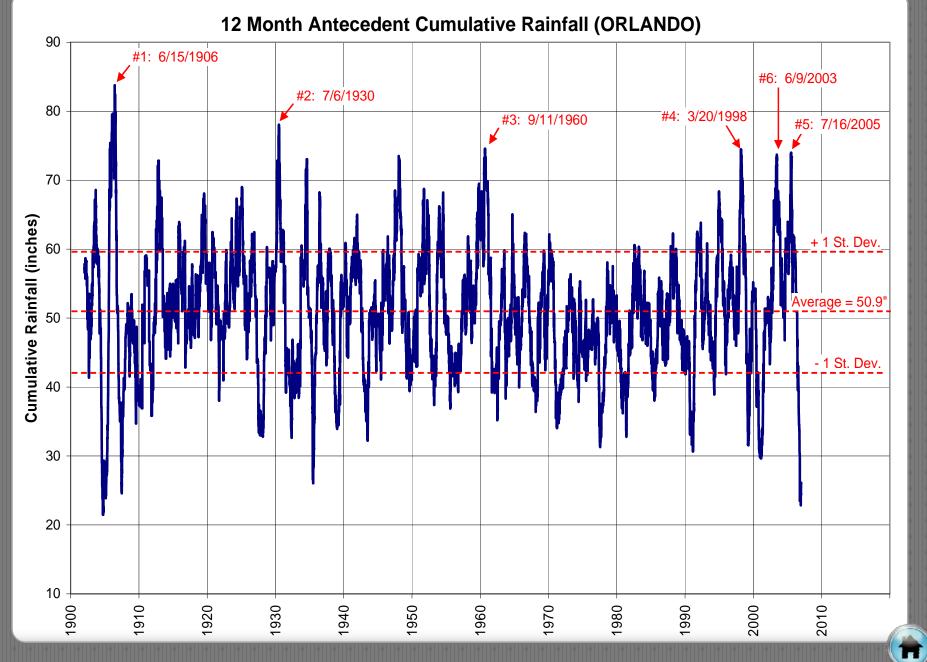


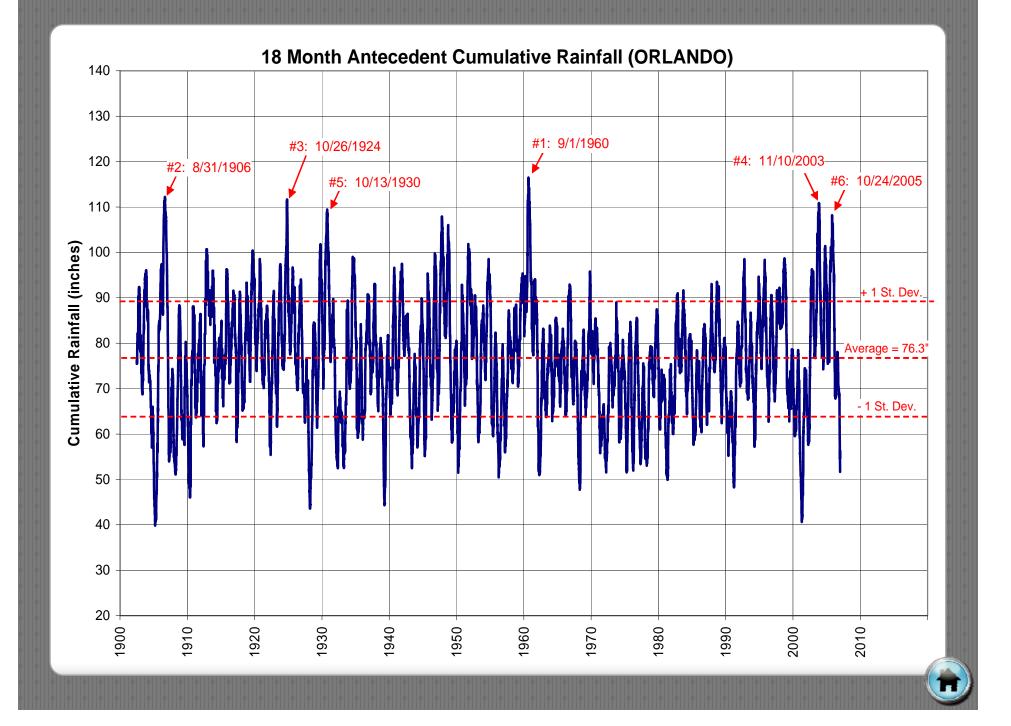
Comparison of Measured Rainfall to FDOT 100-yr / 24-hr Storm Event

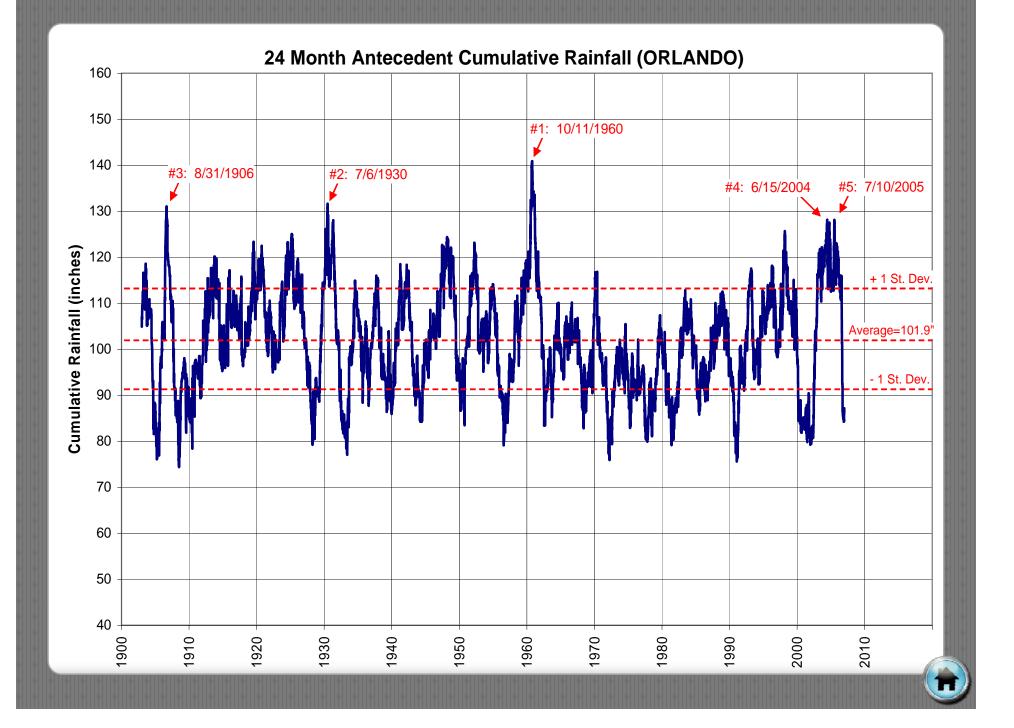
OIA Peak	10-day &	31-day	Rainfall
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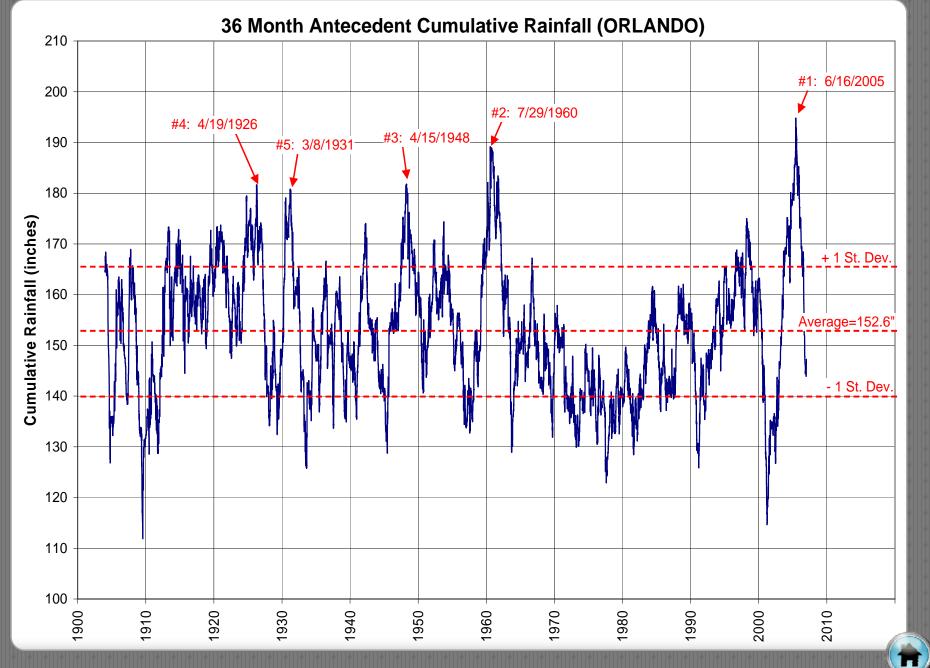
Rank	10-day Antecedent Rainfall (inches)	31-day Antecedent Rainfall (inches)
1	15.25 (6/30/1910)	21.70 9/8/1933
2	14.20 (10/21/1940)	20.50 7/25/1960
3	13.33 (9/16/1945)	20.07 10/28/1915
4	13.31 (9/8/1933)	20.02 6/29/2005
5	13.03 (10/14/2015)	19.43 9/6/2004

FDOT 100-yr/10-day is 16 to 18 inches.







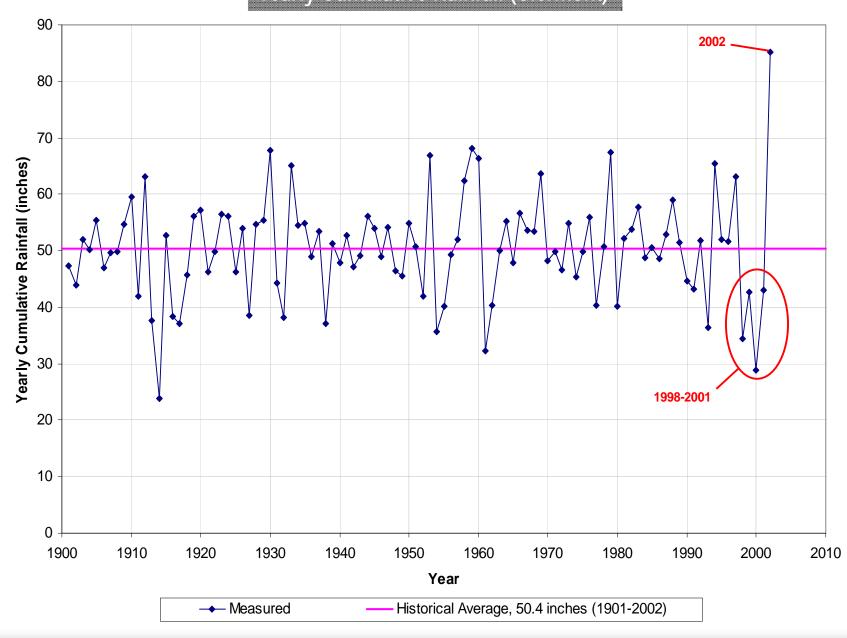


101 Years of Rainfall Data at Clermont Weather Station 1901 - 2002



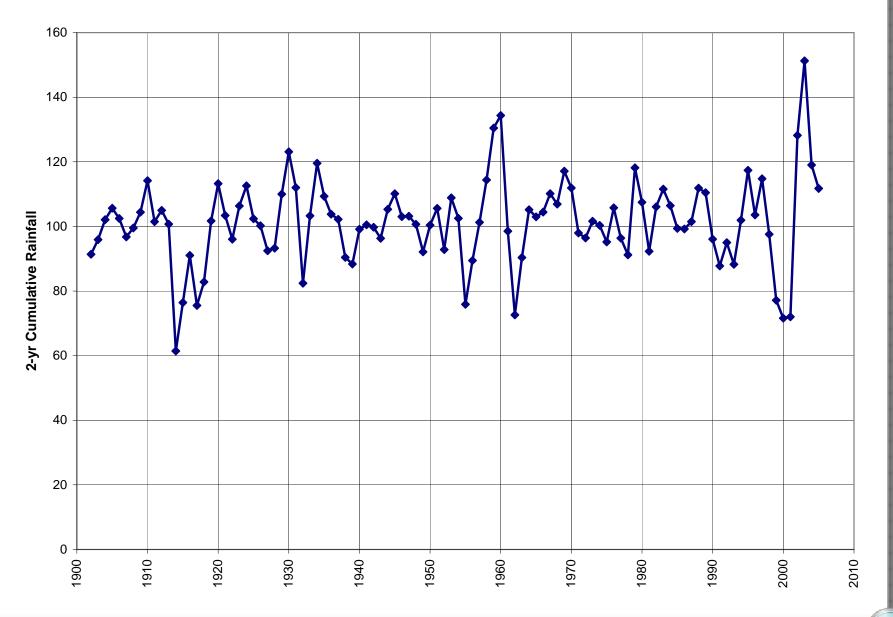
Yearly Cumulative Rainfall (Clermont)



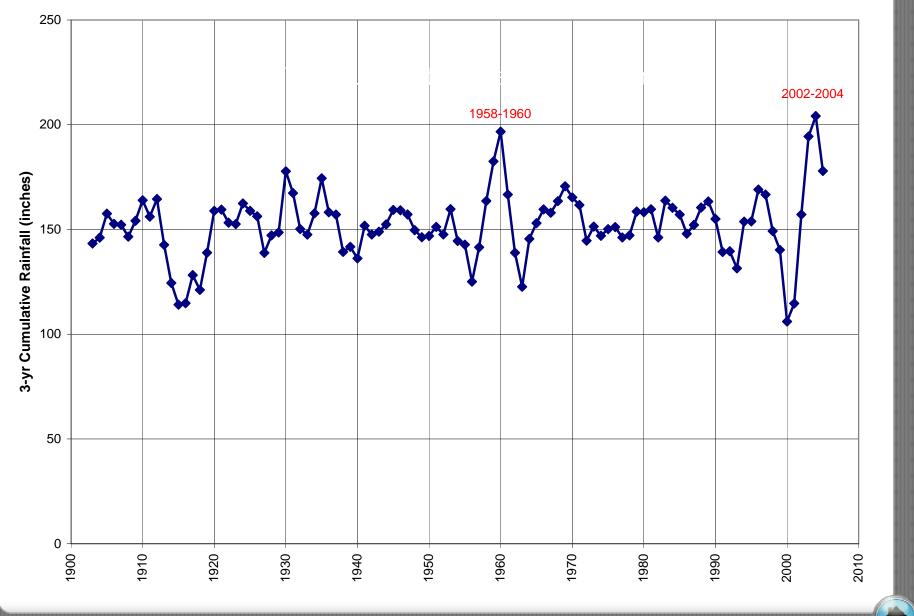


Yearly Cumulative Rainfall (Clermont)

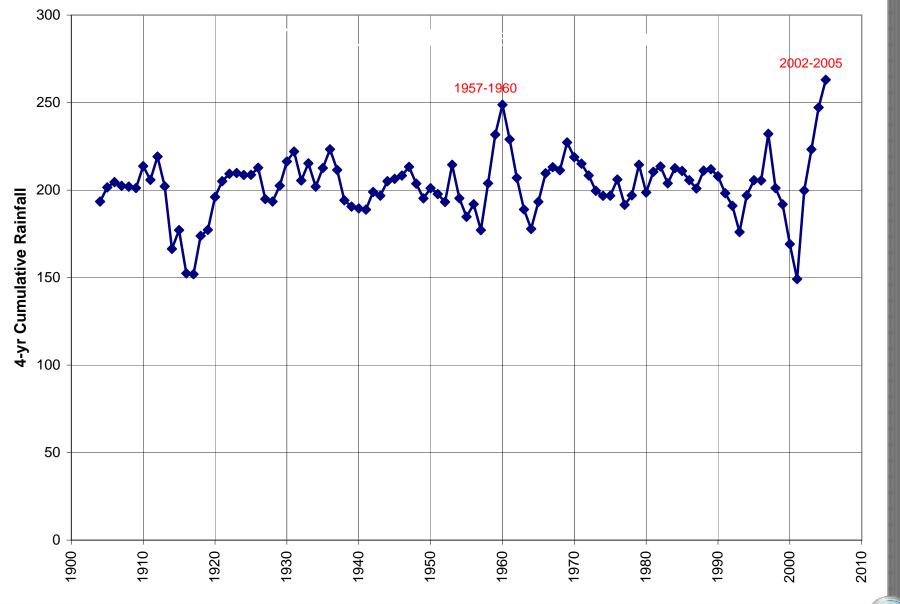
2-Year Cumulative Rainfall (Clermont)



3-Year Cumulative Rainfall (Clermont)

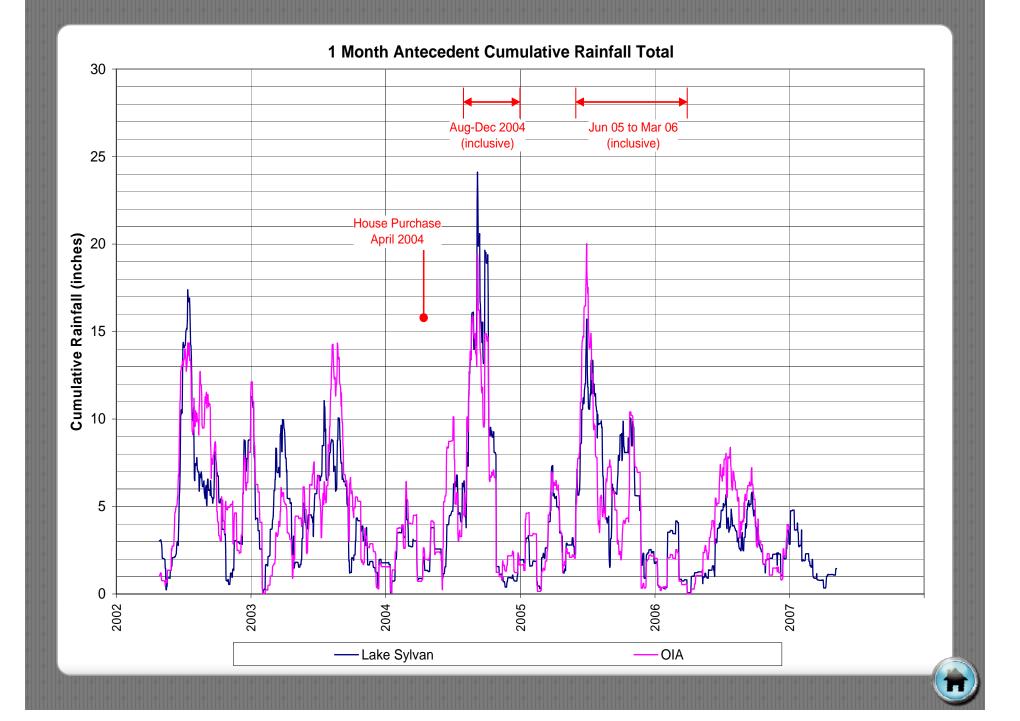


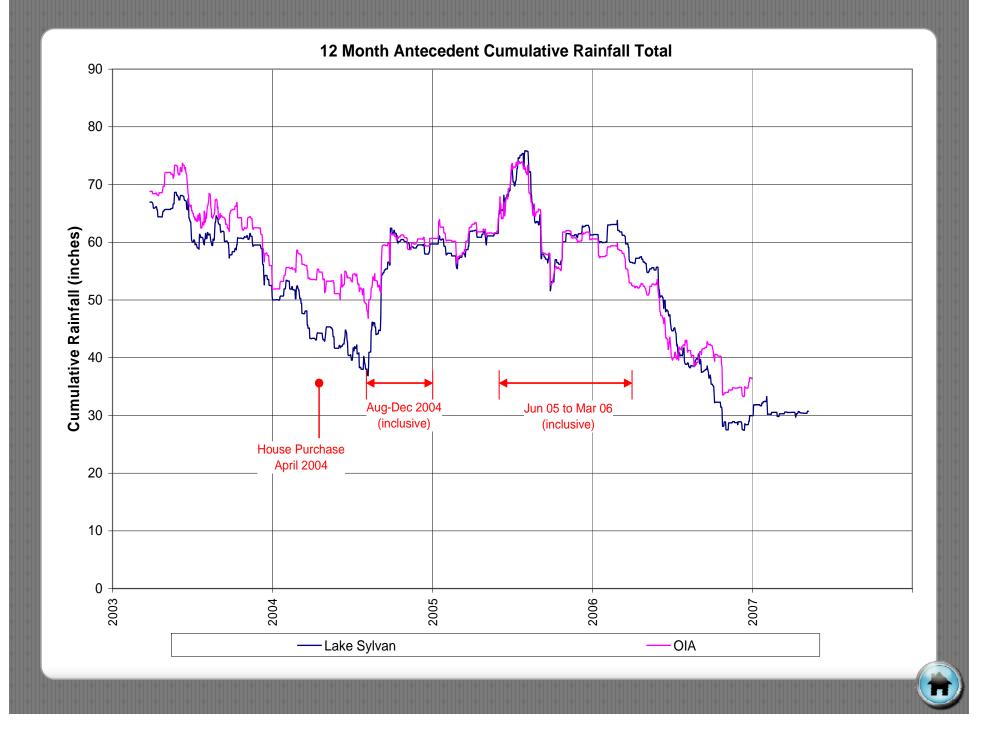
4-Year Cumulative Rainfall (Clermont)

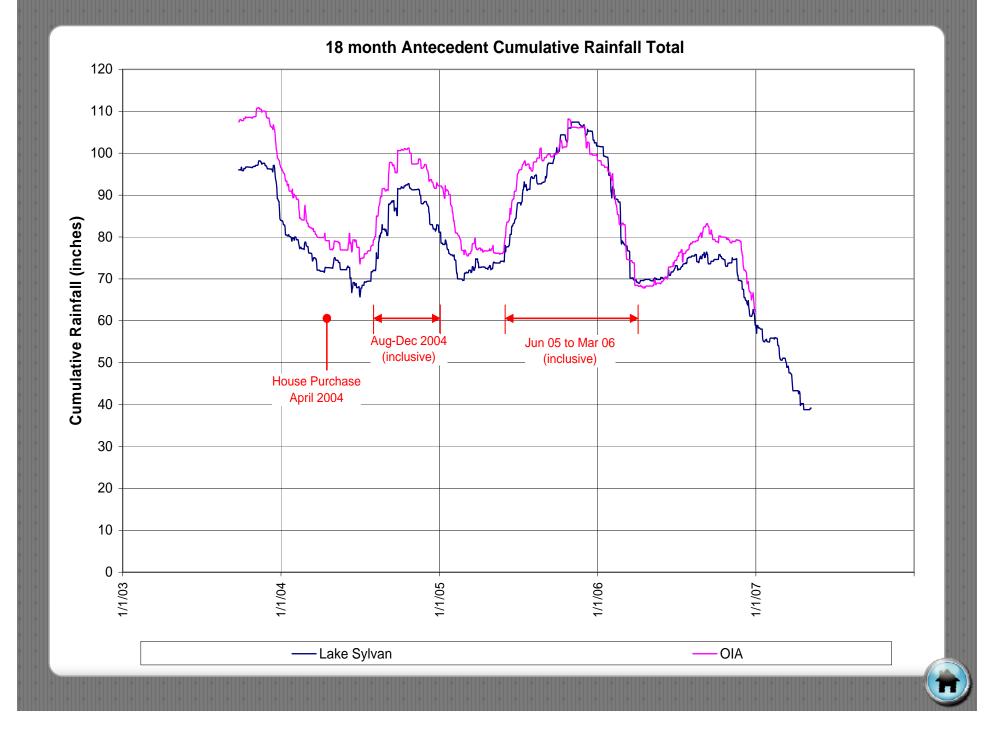


Rainfall at Lake Sylvan

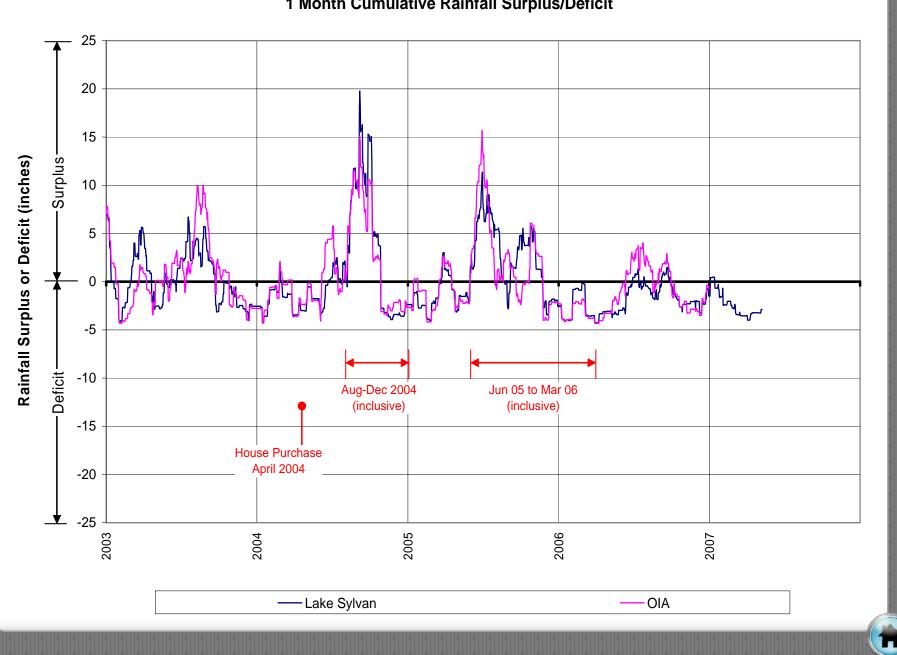
The Lake Sylvan site is located near the Heathrow community in Seminole County. The purpose of this exercise was to compare the rainfall patterns at OIA and Lake Sylvan to see if their trends were consistent from a long term standpoint or vastly different.



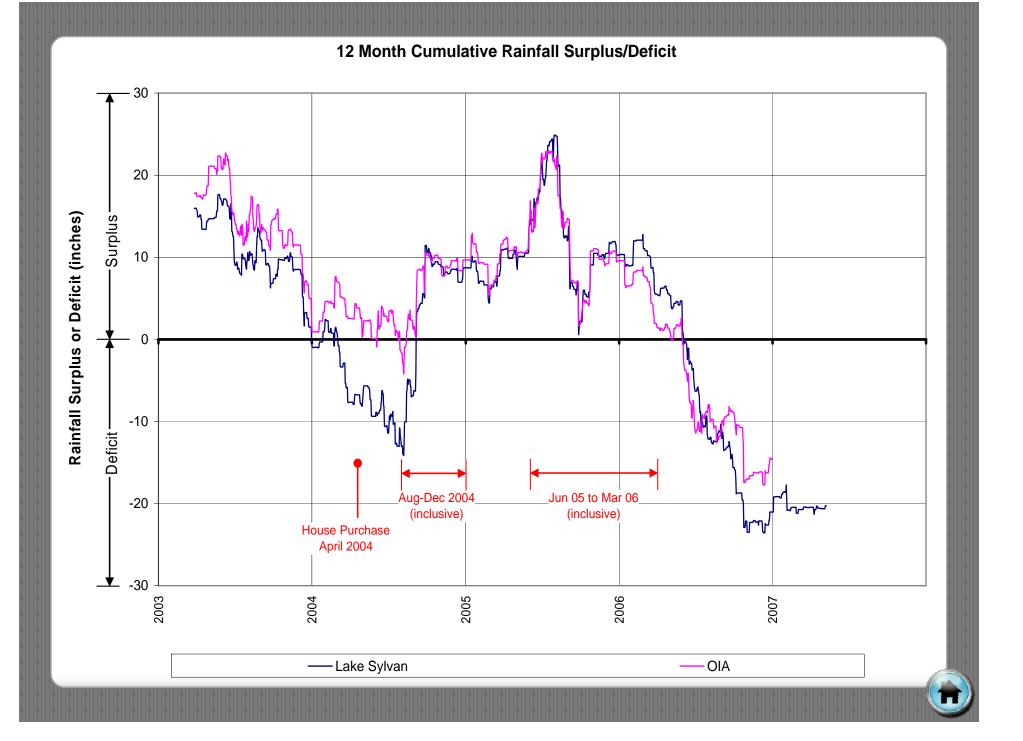




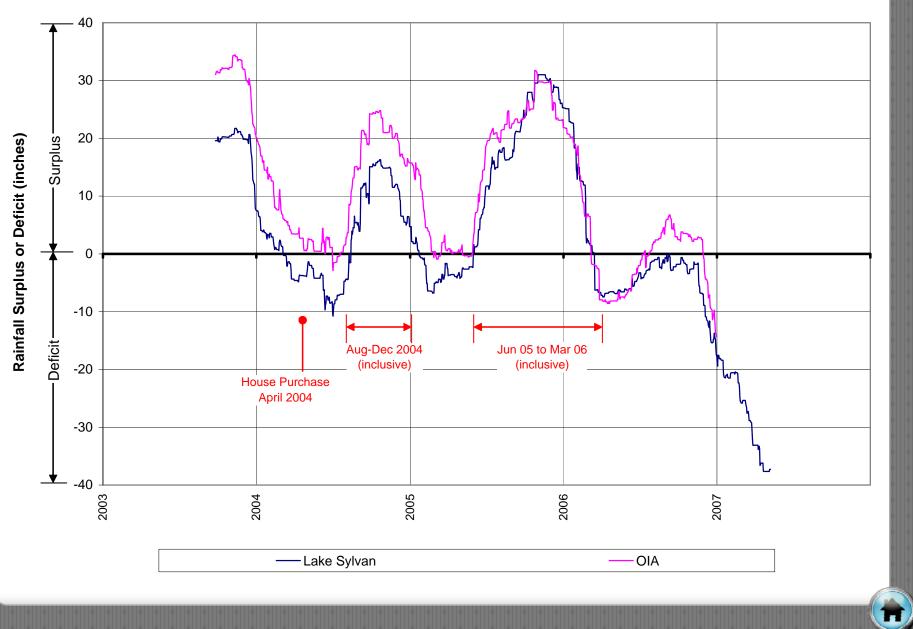
Rainfall Surplus/Deficit at Lake Sylvan



1 Month Cumulative Rainfall Surplus/Deficit



18 Month Cumulative Rainfall Surplus/Deficit



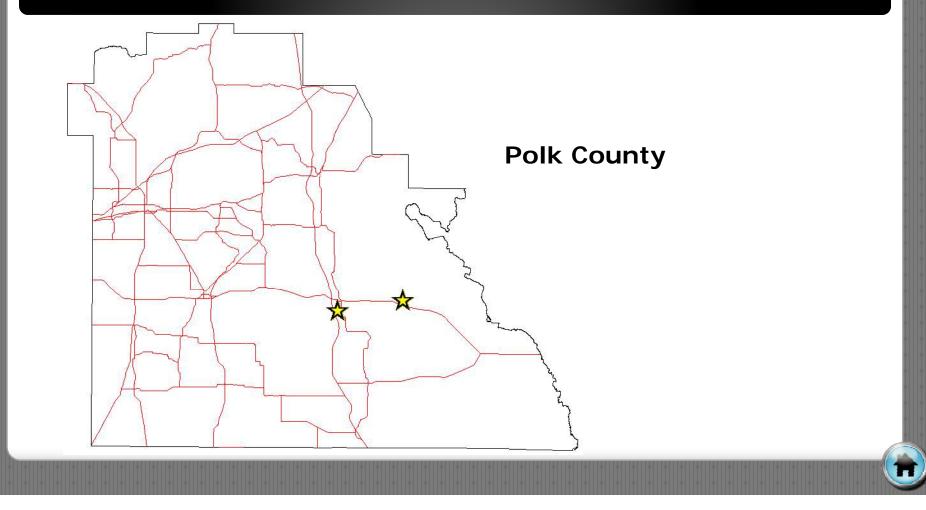
Part 2

Applicability of Current Regulatory Criteria for Ensuring Flood Protection in Land-Locked Drainage Systems

S	SUMMARY OF REGULATORY CRITERIA FOR LAND-LOCKED BASINS					
Agency	Initial Stage for routing	Design Storm Event to compute runoff volume	Recovery Criteria			
SWFWMD	stage after 36 hr of recovery following slug loading of water quality volume. if dry, seasonal high water table	100 yr/24 hr	none			
SJRWMD	the pond bottom or the elevation at which the water quality volume is recovered to; on a case by case basis, the seasonal high water table may be used	on a case by case basis, the 100 yr/24 hr storm may be	14 days on a case by case basis, back to back storms may be analyzed if full recovery cannot be achieved in 14 days			
SFWMD	average wet season water table	100 yr/72 hr	no separate criteria for land locked basins since there are so few in SFWMD			
SRWMD	seasonal high water table	critical duration but usually the critical one for maximum runoff volume is: 100 yr/240 hr storm	50% of the retention volume to be recovered in 7 days, with the total volume to be available in 30 days			
NWFWMD	seasonal high water table	25 yr/96 hr	None			
FDOT	Lowest elevation of available storage above the seasonal high water table	critical duration/frequency that yields highest pre-post runoff volume. max duration of 240 hr	50% of the retention volume to be recovered in 7 days, with the total volume to be available in 30 days			
FEMA	seasonal high water table	100 yr/96 hr storm, or 100 yr/24 hr preceded by a mean annual storm (2.33 yr/24 hr)	none			
Orange County	seasonal high water table not more than 50% of water quality volume	100 yr/24 hr	14 day recovery natural seepage or bleed-down			

Some Examples of Recent Flooding Problems

Lake Belle, Tractor Lake, & Saddlebag Lake



Saddlebag Lake





Saddlebag Lake



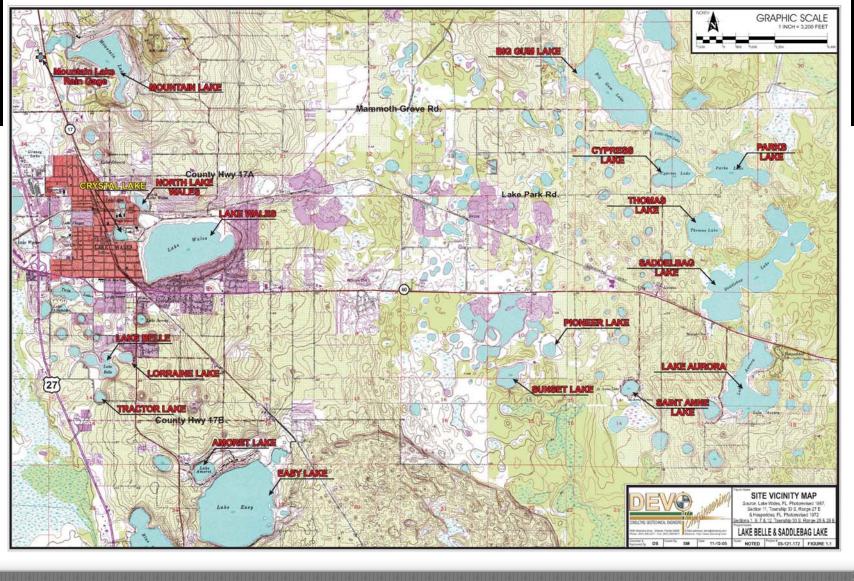


Lake Belle

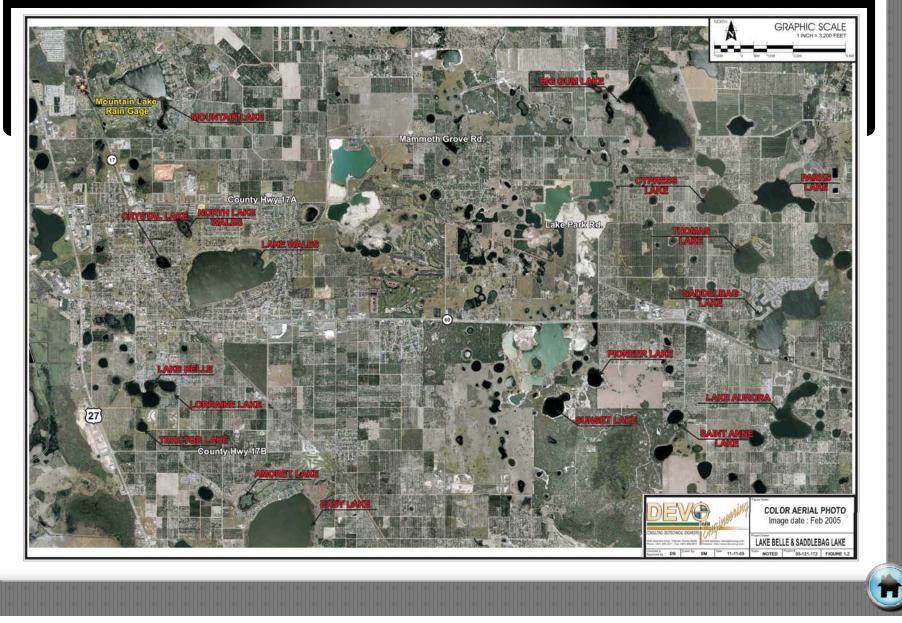




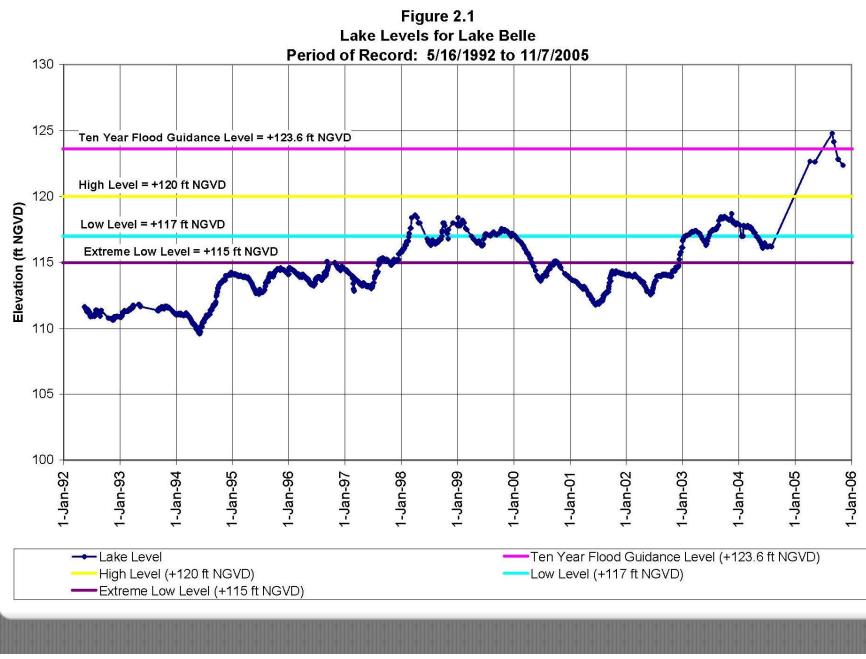
Site Vicinity Map



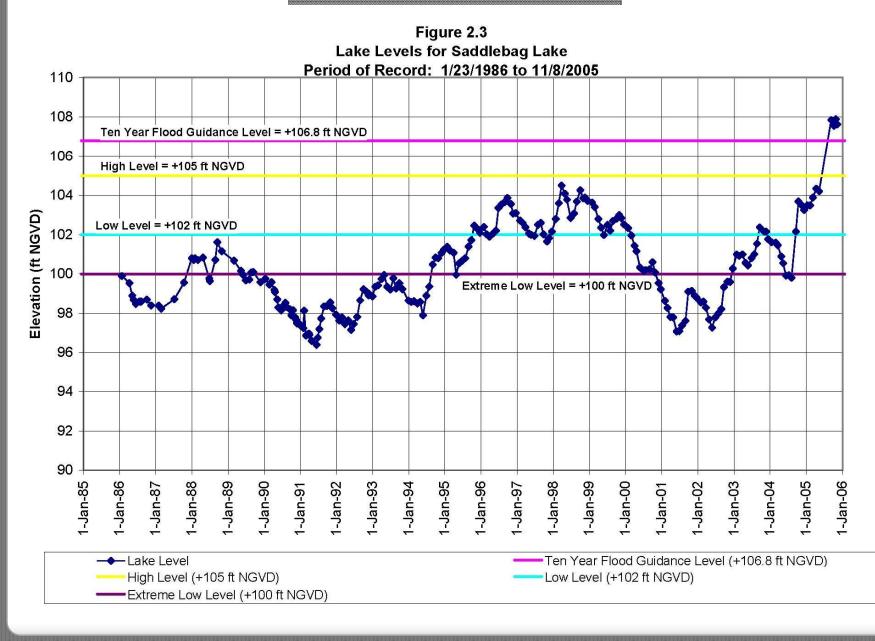
Aerial Map



Lake Levels for Lake Belle



Lake Levels for Saddlebag Lake





1-yr Antecedent Rainfall

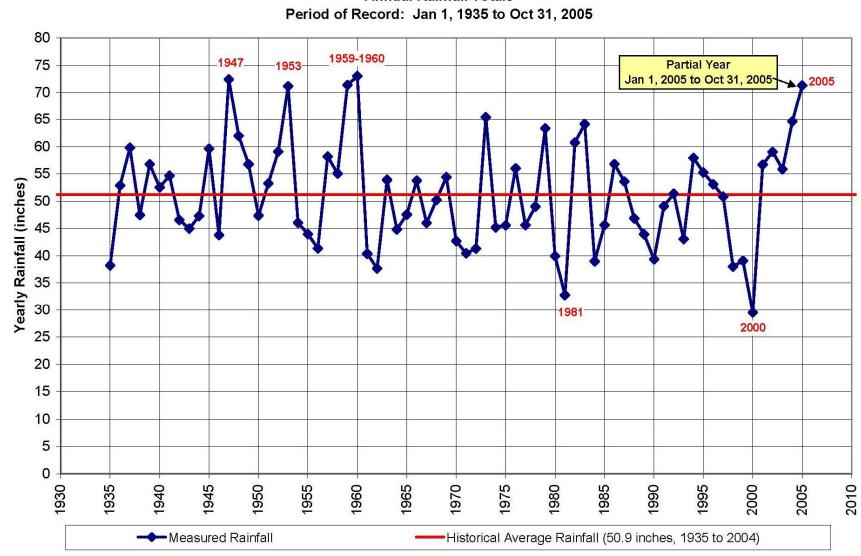
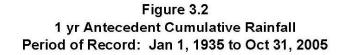
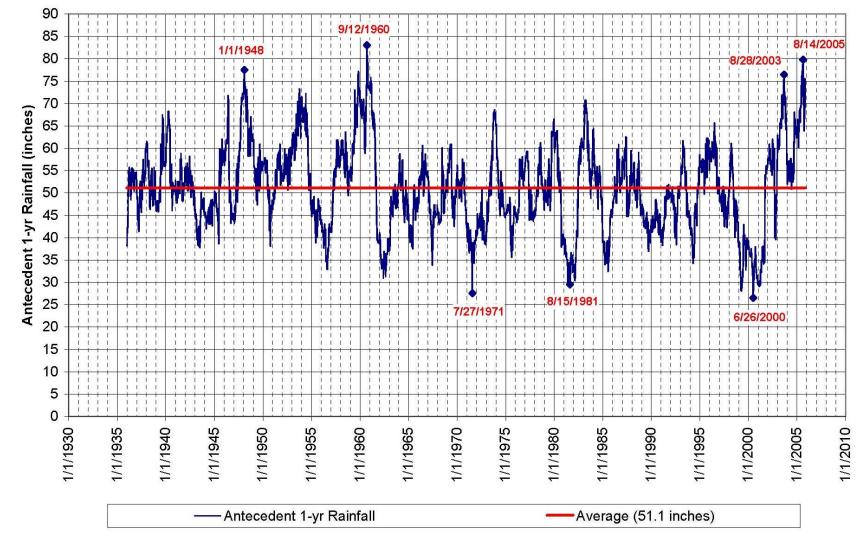


Figure 3.1 Annual Rainfall Totals Period of Record: Jan 1. 1935 to Oct 31. 2005



1-yr Antecedent Rainfall





2-yr Antecedent Rainfall

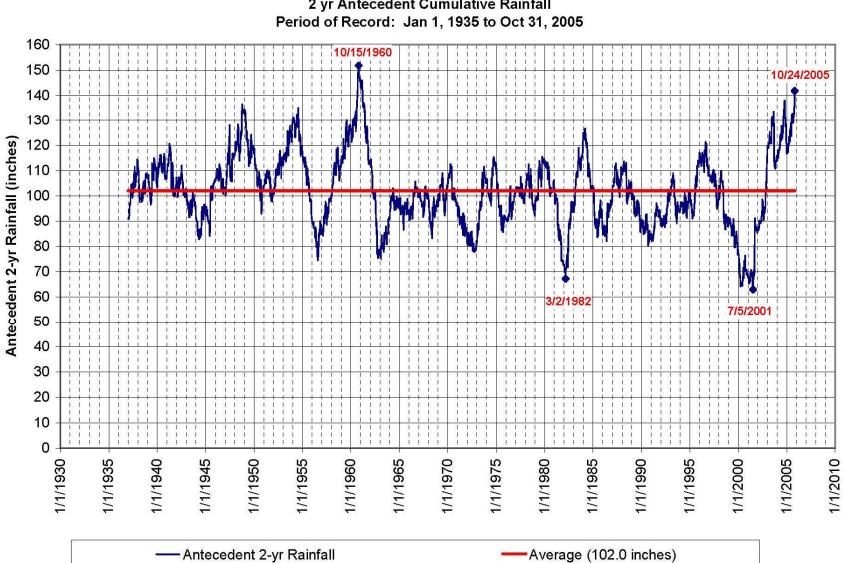
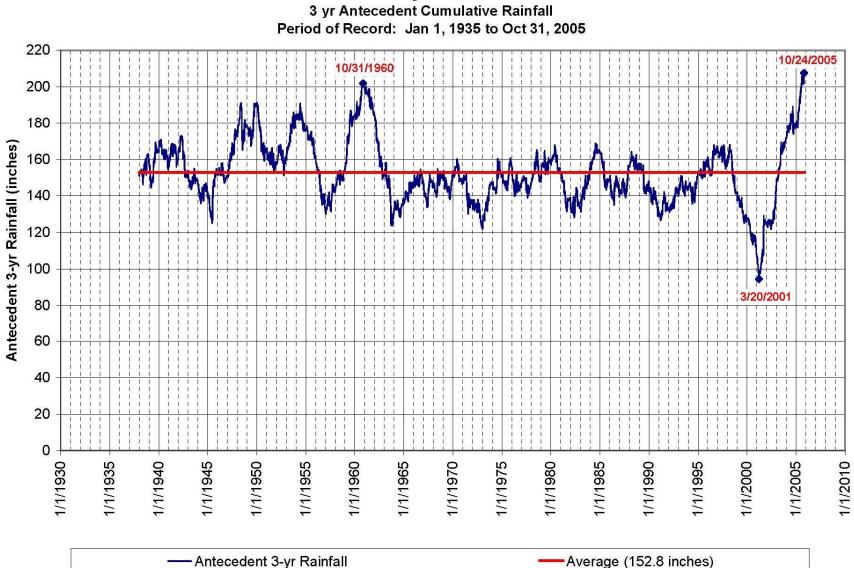


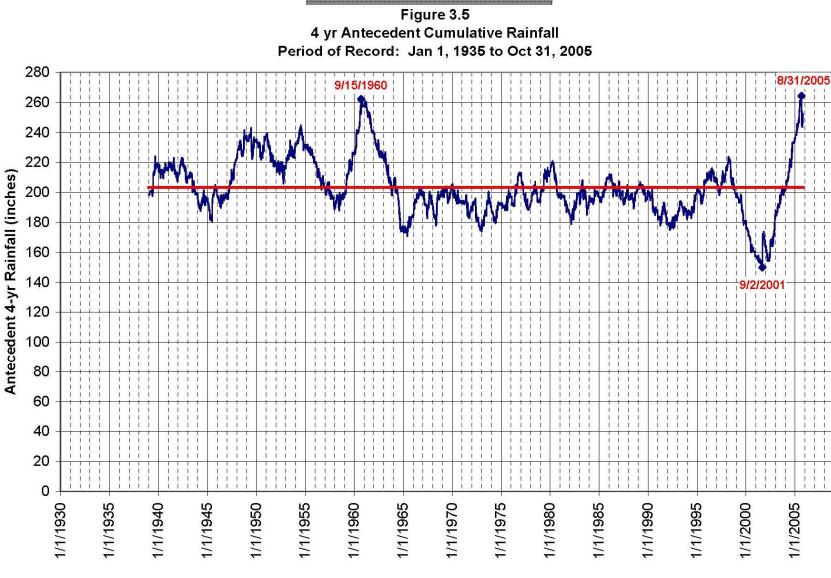
Figure 3.3 2 yr Antecedent Cumulative Rainfall

3-yr Antecedent Rainfall

Figure 3.4



4-yr Antecedent Rainfall

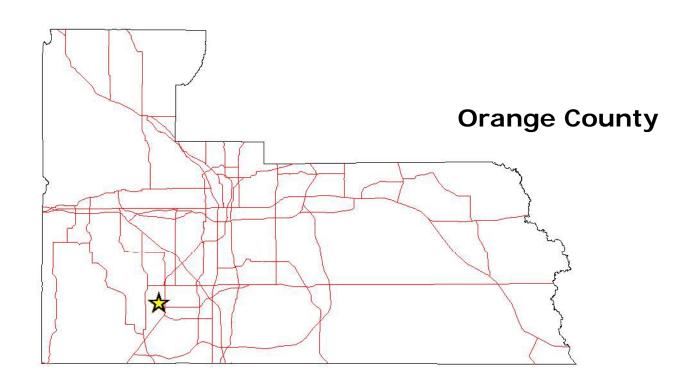


— Antecedent 4-yr Rainfall

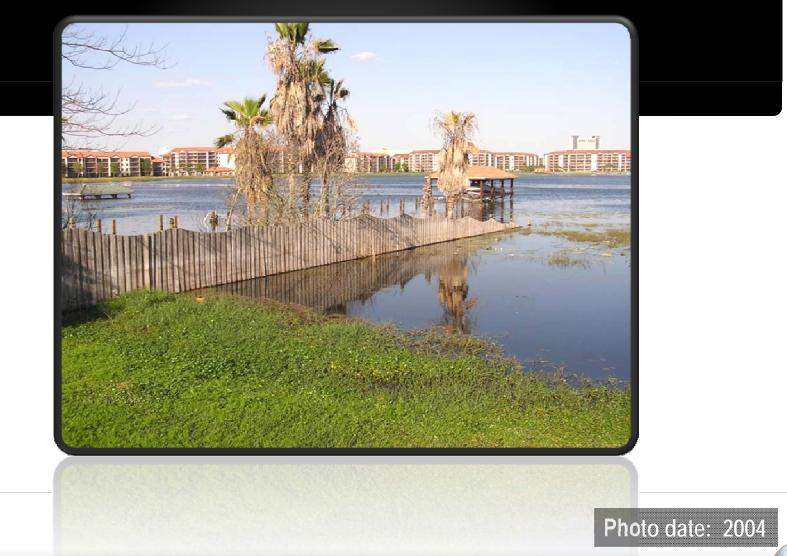
-Average (203.3 inches)

1/1/2010

Big Sand Lake



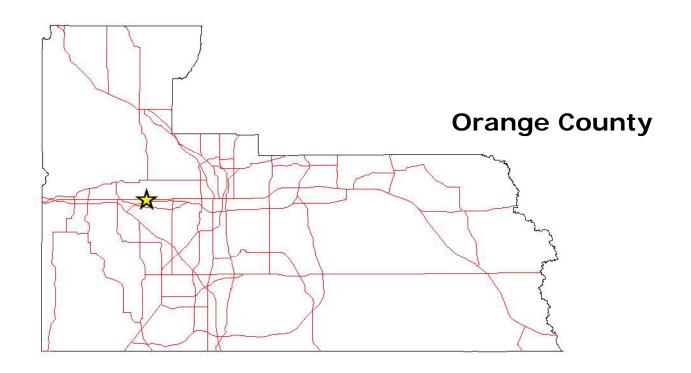
Big Sand Lake



Big Sand Lake



Photo date: 2004





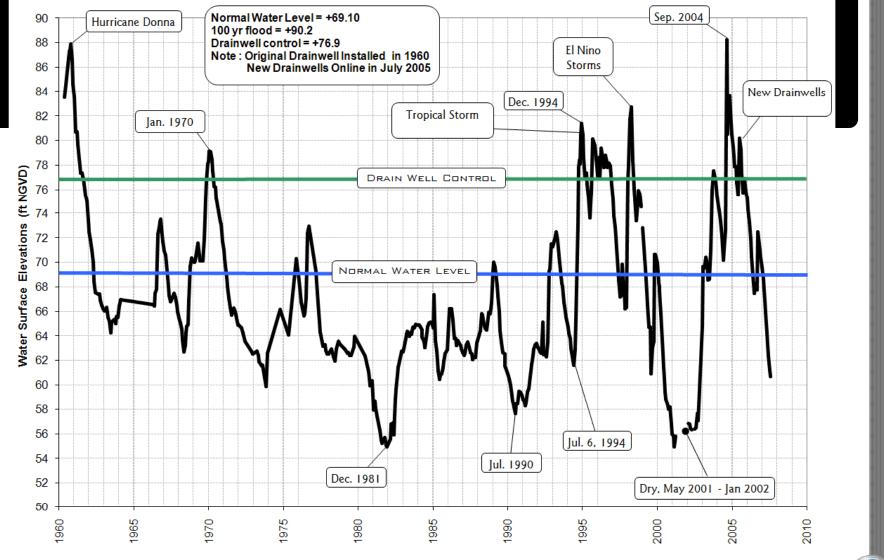
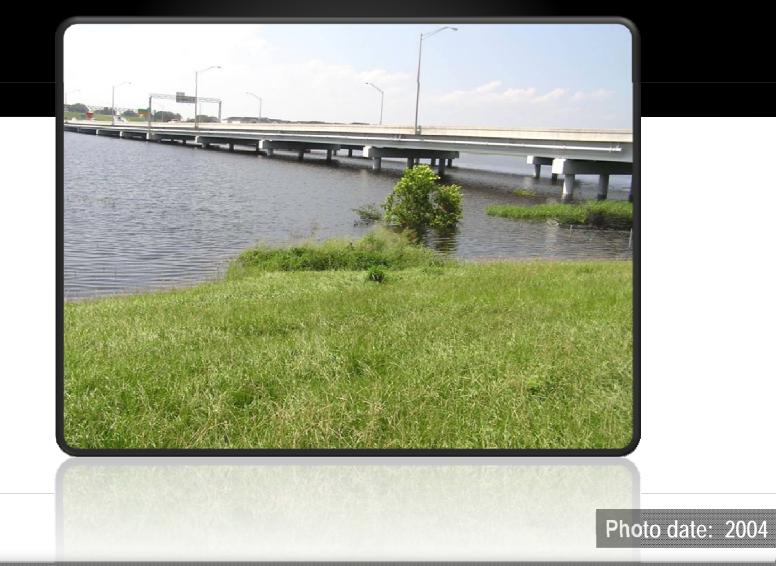




Photo date: March 1998

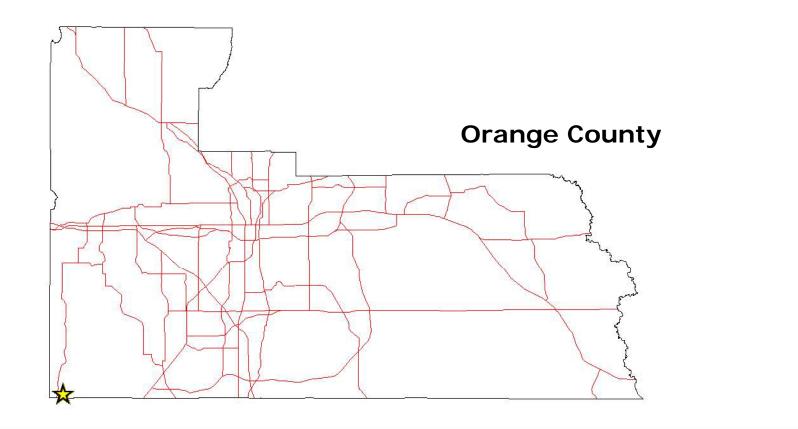


Photo date: March 1998





Lake Rexford and Lake Osage



Lake Rexford and Lake Osage



Lake Rexford and Lake Osage

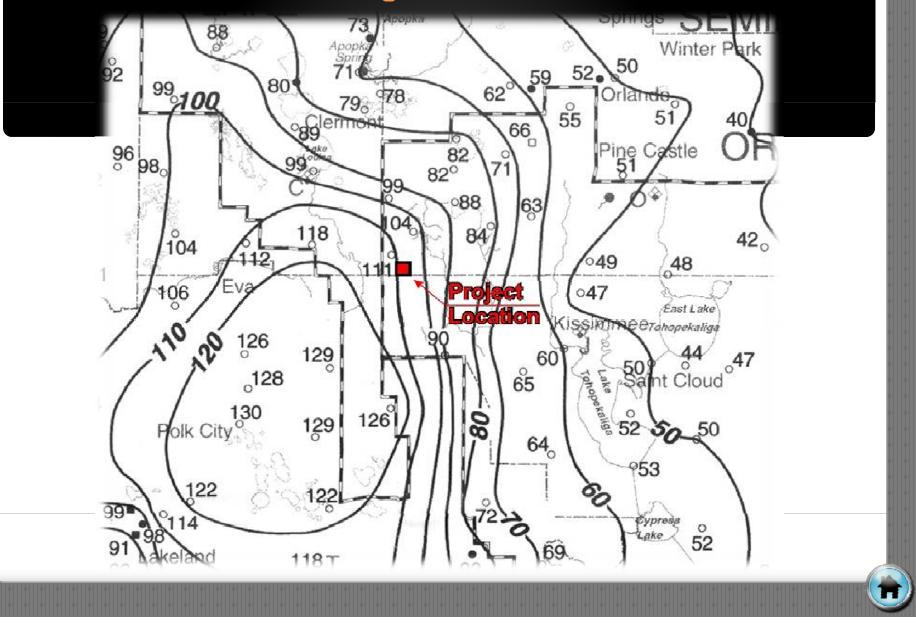


Photo date: 2003

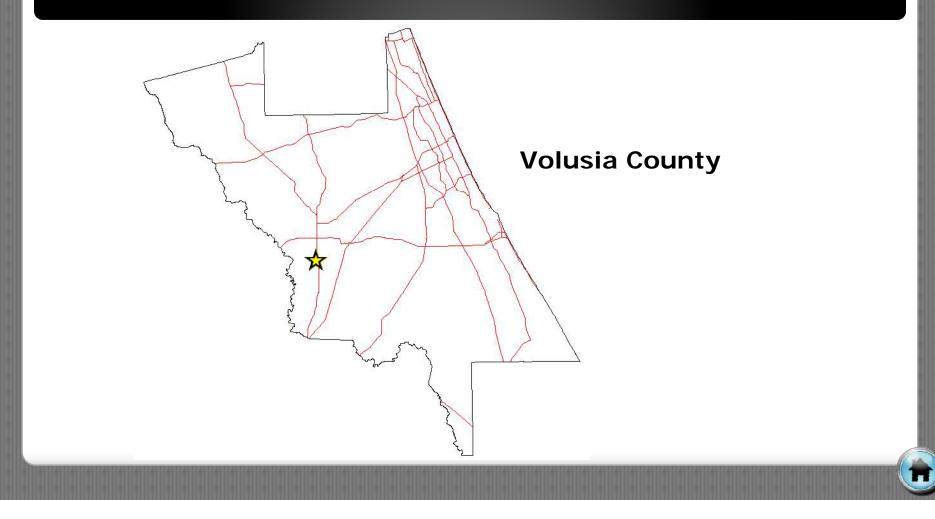
Lake Rexford and Lake Osage



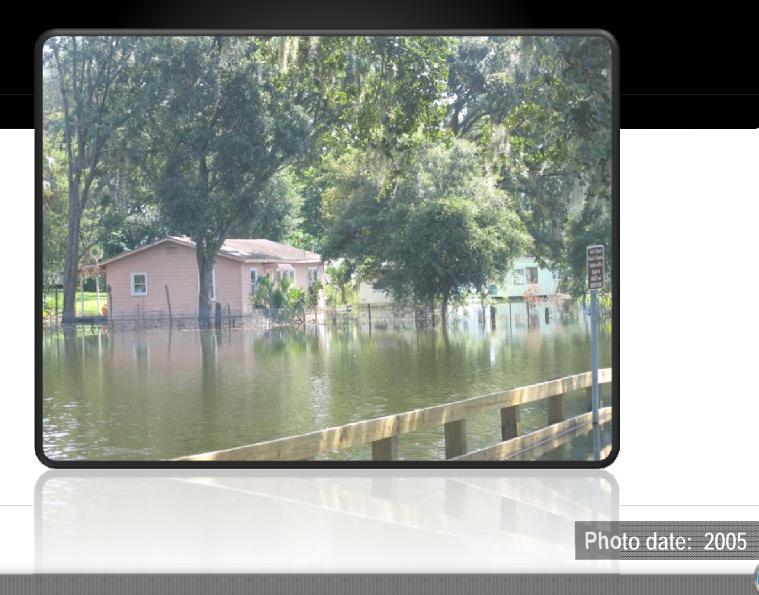
Lake Rexford and Lake Osage Potentiometric Surface Contours



Calvin Street and Crystal Cove



Calvin Street Depression, Deland Area



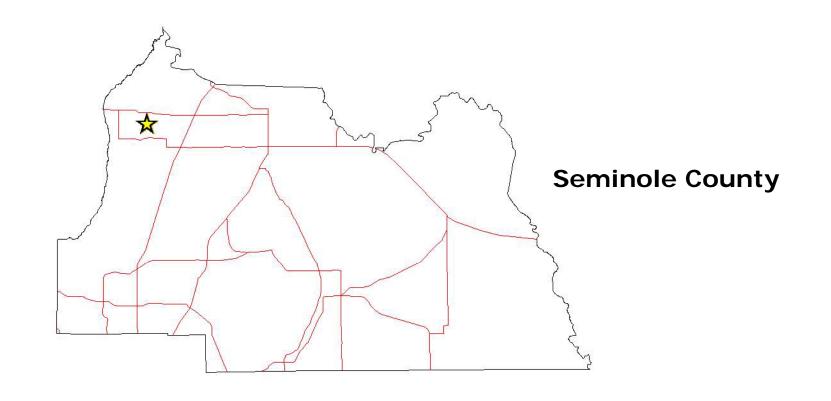


Crystal Cove, Deland Area

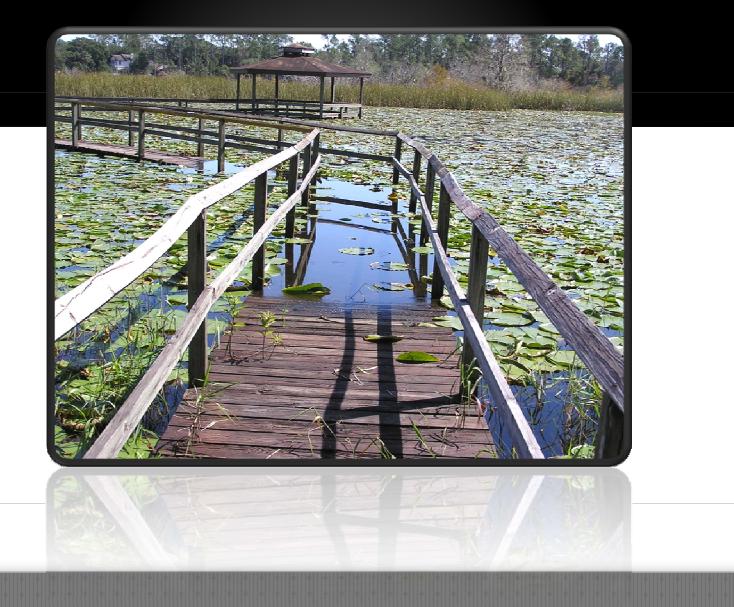


Photo date: 2005

Lake Sylvan



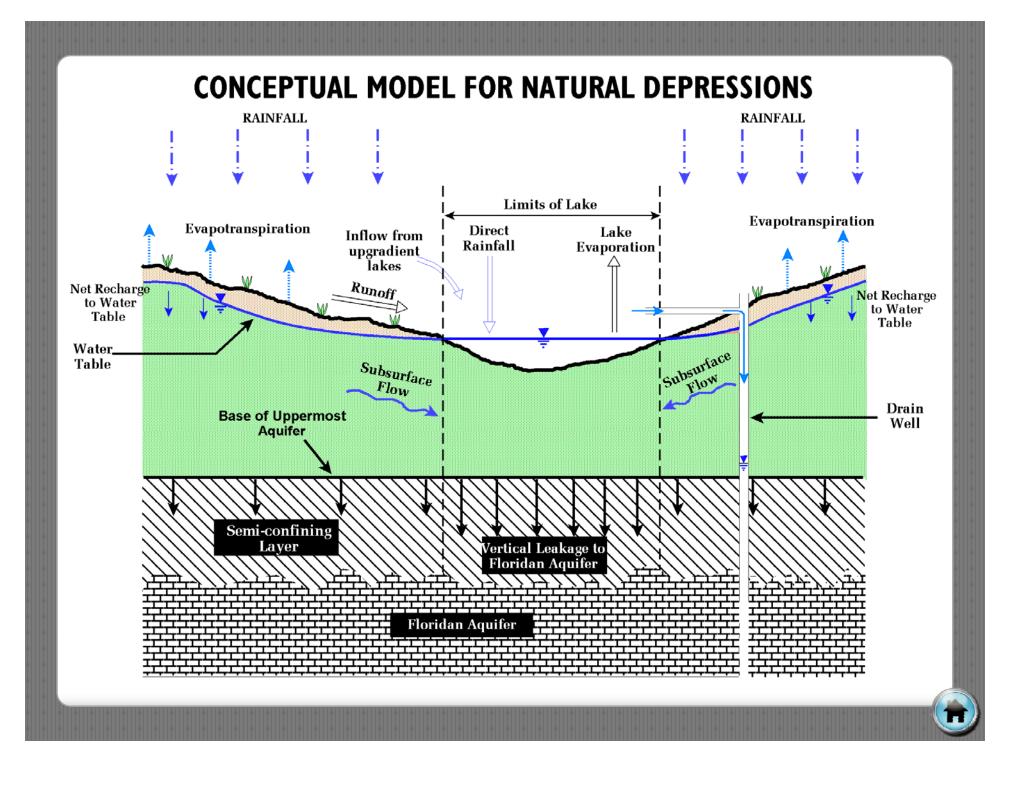
Lake Sylvan

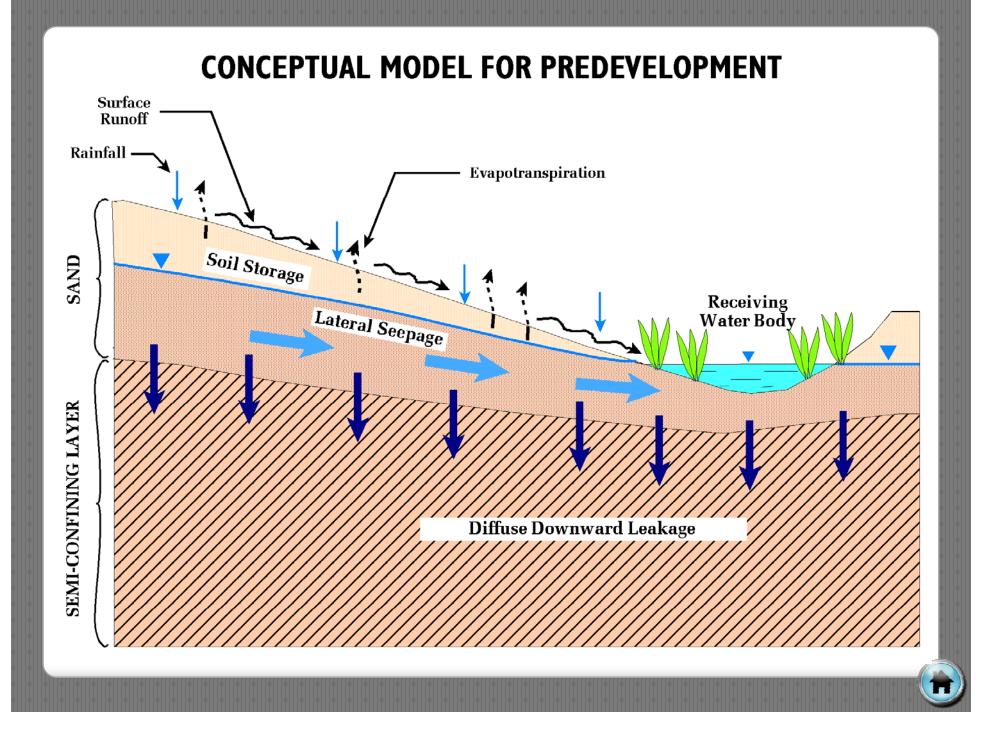


Part 3

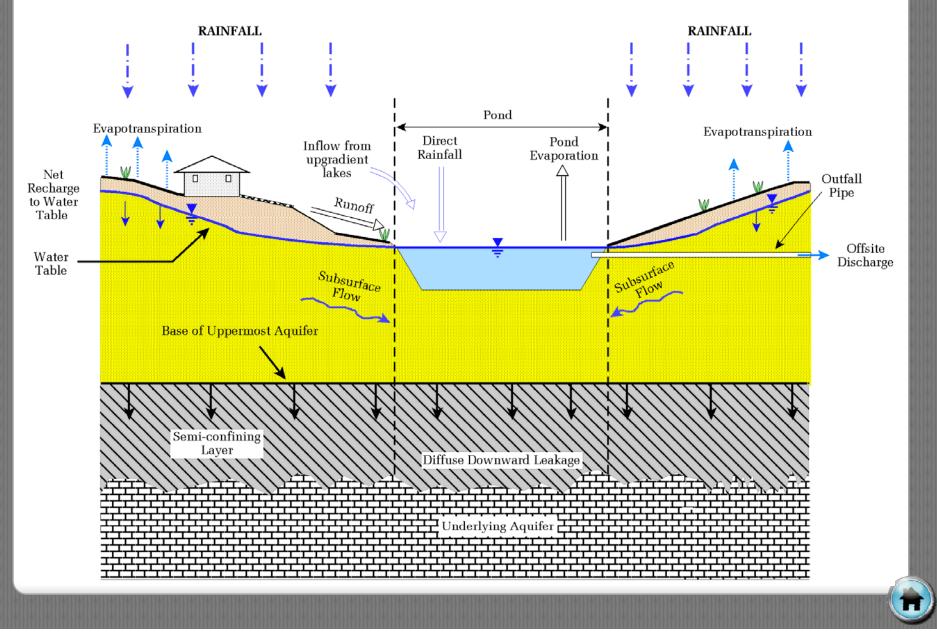
Long-term and short-term continuous simulation modeling of stormwater management systems. Is it time for its integration in stormwater management criteria? Are the tools & technology available to practitioners? Continuous Simulation Modeling of Stormwater Ponds, Lakes, & Wetlands:

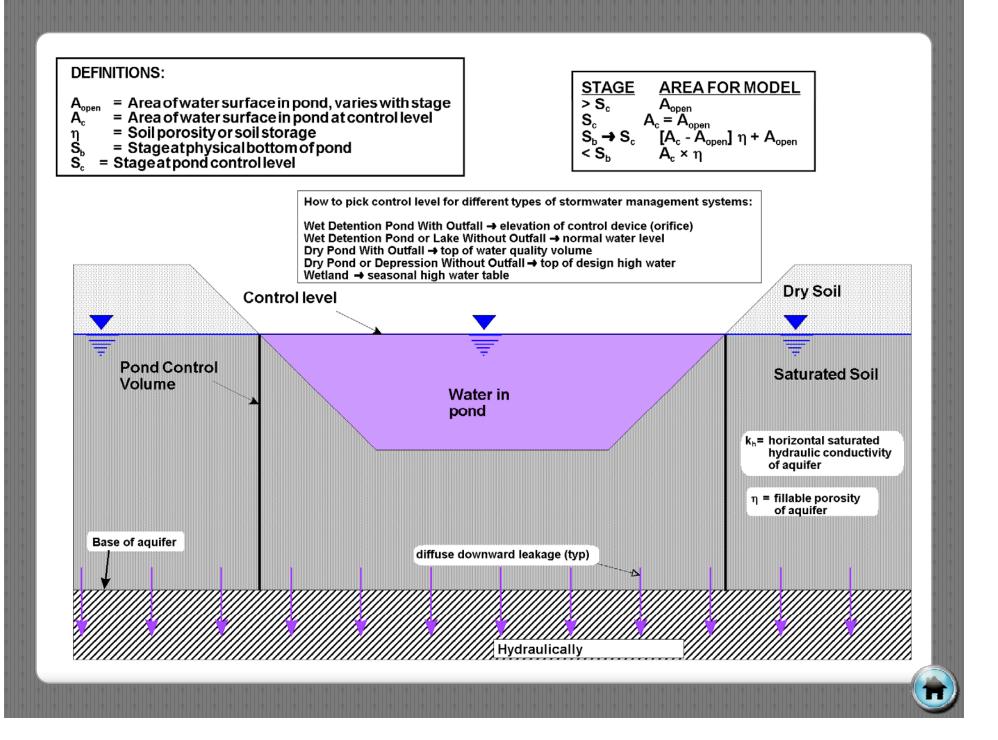
BUILT-IN INTO PONDS 3.2 – the continuous simulation hydrograph, what additional parameters do we need to consider?



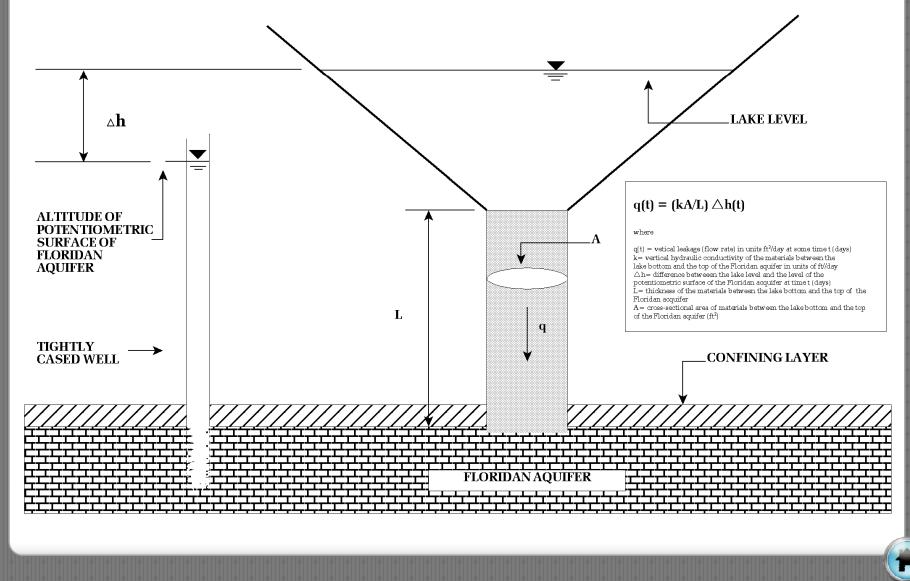


CONCEPTUAL MODEL FOR POSTDEVELOPMENT









CONTINUOUS SIMULATION MODELING: CONCEPTUAL MODELS DIFFUSE DOWNWARD LEAKAGE - THINK ABOUT THIS FIRST

- Simple models are those where the vertical recharge rate (aka "diffuse downward leakage") is uniform with time. There are actual sites like this in the areas of very low recharge (for example, East Orange County).
- Less simple models are those where the diffuse downward leakage changes markedly with time based on rainfall and the water level (pot surface) in the underlying Floridan aquifer. These models require some calibration to back-compute the daily or monthly recharge rate. All other parameters are known.

Part 4

Some Screen Shots of PONDS 3.2 Software Continuous Simulation Hydrograph Generator

🖣 Continuous Simula	lation 🛛	<
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Scenario 7		
Hydrograph Type Cont	ntinuous Simulation Clone	
Description Post	st - Wet years: Jan 1, 1994 to Sep 21, 1998 <- Auto Describe	
	Rainfall 🗋 🚔 🚽	
Modflow Options	Rainfall	_
Rainfall	Data format Date range	
Runoff	Units English	
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Artificial Recharge	(incres)	
Upgradient Flow	1 Jan 1, 1994 1.20 2 Jan 2, 1994 0.20	
Pumping	2 Jan 2, 1994 0.20 3 Jan 3, 1994 0.30	
	4 Jan 4, 1994 0.00	
Summary	5 Jan 5, 1994 0.00	
	6 Jan 6, 1994 0.00	
	7 Jan 7, 1994 0.00 🗸	
	Ok Cancel	1

Elle Summary Menu Scenario 7 Hydrograph Type Continuous Simulation Post - Wet years: Jan 1, 1994 to Sep 21, 1998 Modflow Options Rainfall Runoff Lake Surface Water Basin Ground Water Basin Season Definition for CN Adjustment Units English Lake Area (acres) 0.708 Upgradient Flow Pumping Summary	Continuous Simulation	×
Hydrograph Type Continuous Simulation Clone Description Post - Wet years: Jan 1, 1994 to Sep 21, 1998 <- Auto Describe <table> Modflow Options Runoff Rainfall Lake Surface Water Basin Ground Water Basin Season Definition for CN Adjustment Units English Leakage Artificial Recharge Upgradient Flow Pumping</table>	Eile Summary Menu	
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Eile Summary Menu	
	Image: Simulation Image: Clone Wet years: Jan 1, 1994 to Sep 21, 1998 <- Auto Describe
Modflow Options	Runoff 🗋 🖆 🖬
Rainfall	Lake Surface Water Basin Ground Water Basin Season Definition for CN Adjustment
Runoff	Units English
Evap/ET	Total area of drainage basin, including lake (acres)
Leakage	Directly Connected Impervious Area (acres) 3
Artificial Recharge	Impervious area within basin where there are no E.T. losses (acres)
Upgradient Flow	Curve Number for non-DCIA Area (AMC I) 51
Pumping	Curve Number for non-DCIA Area (AMC II) 70
Summary	Curve Number for non-DCIA Area (AMC III) 85
	Curve Number for DCIA 98
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🖣 Continuous Simulati	ion 🔀
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Modflow Options	Runoff 🗋 🖨 🖬
Rainfall	Lake Surface Water Basin Ground Water Basin CN Adjustment
Runoff	Date Format Calendar year, monthly
Evap/ET	Wet/Dry Seasons
Leakage	
Artificial Recharge	Date Season
Upgradient Flow	Jan dormant Feb dormant
Pumping	Mar dormant
Summary	Apr dormant
	May dormant Jun growing
	Jul growing
	Ok Cancel

Continuous Simulation 🛛	
Summary Menu	
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Modflow Options	Ī
Rainfall <u>Evapotranspiration (ET) Ratio</u>	
ET (impervious) / ET (pervious) [%]	
Bunoff Evaporation and Evapotranspiration (ET)	
Evap/ET Date Format Calendar year, monthly	
Leakage Units English 💌	
Artificial Recharge Evaporation and E.T.	
Upgradient Flow	
Pumping Date Evaporation E.T.	
Summary (inches) (inches) Jan 2.20 1.97	
Feb 2.50 1.85	
Mar 3.90 2.68	
	1
OkCancel]

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Modflow Options	Leakage
Rainfall	Leakage Model Constant Rate
Runoff	Units English 💌
Evap/ET	Leakage Inside Pond (inch/yr) 12
Leakage	Leakage Outside Pond (inch/yr) 12
Artificial Recharge	
Upgradient Flow	
Pumping	
Summary	
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🖻 Continuous Simu	ulatior				
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Modflow Options		Summary	1		
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Runoff		Summary			
Evap/ET			Total (ft®)	Total (inches)	
Leakage		Summary of outside recharge water balance components			
Artificial Recharge		Total direct rainfall outside pond		+291.5	
		Recharge from septic tanks	<u> </u>	0	
Upgradient Flow		Recharge from other baseflows		0]
Pumping		Runoff from DCIA		-76.62952	
Summary		Runoff from non-DCIA		-19.81175	
		Diffuse vertical leakage		-56.67867	
		Evapotranspiration loss Net recharge to water table during simulation		+11.43406	
		Necrecharge to water table during simulation		+11.43406	
			1		-
				Ok	Cancel

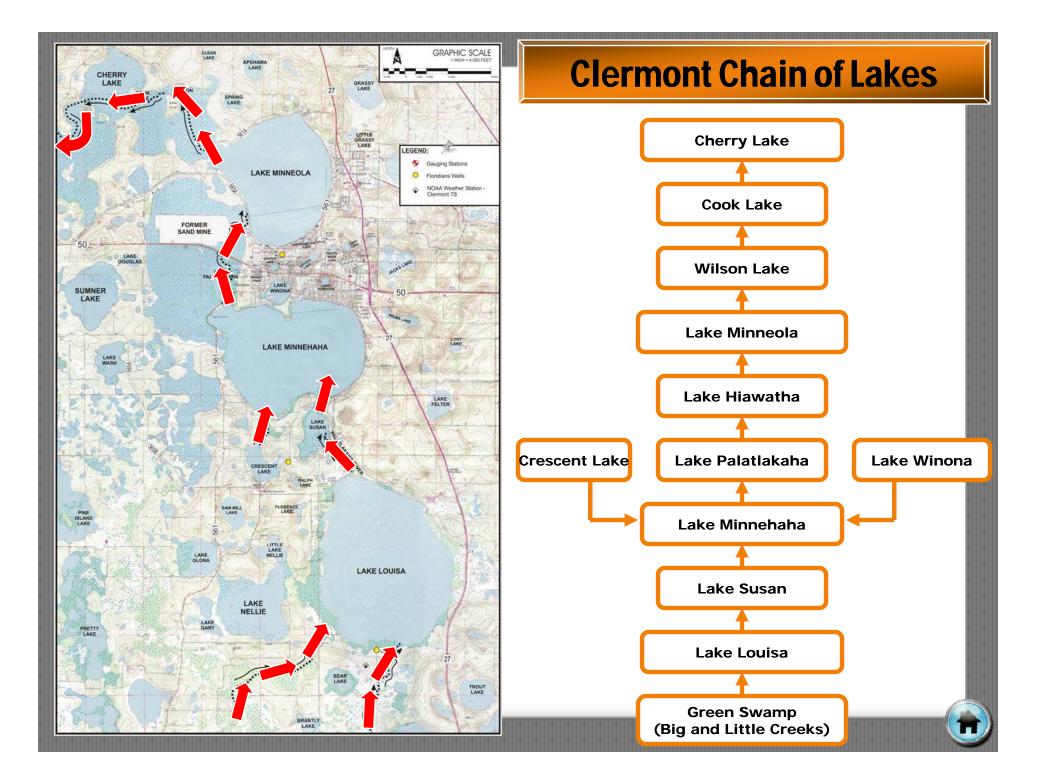
CONTINUOUS SIMULATION MODELING: DOES IT WORK?, HAS IT BEEN TESTED?

LET US LOOK AT SOME EXAMPLES OF ACTUAL MODELING PROJECTS AND COMPARISONS BETWEEN MEASURED AND PREDICTED LEVELS

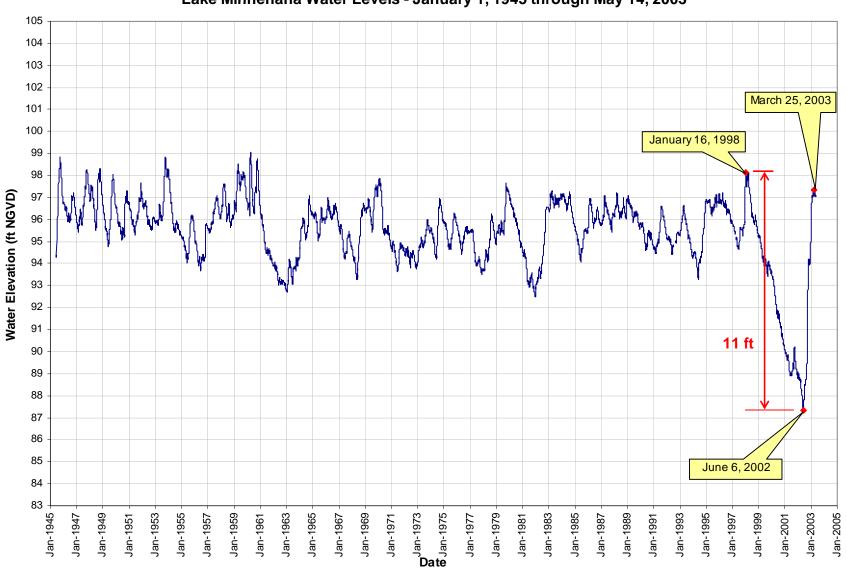
Example: Clermont Chain of Lakes



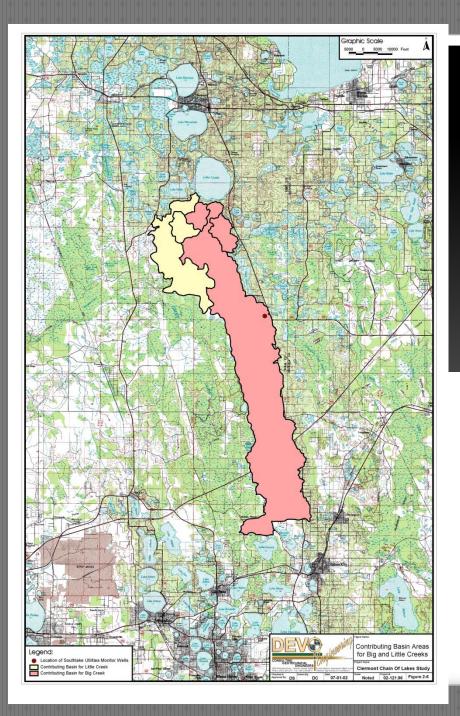
Lake Minneola, 6/10/2002



Lake Minnehaha Water Levels



Lake Minnehaha Water Levels - January 1, 1945 through May 14, 2003



Location of Big Creek Recharge Basins

- Approximately 39,000 acres
- Running parallel to Lake Wales Ridge

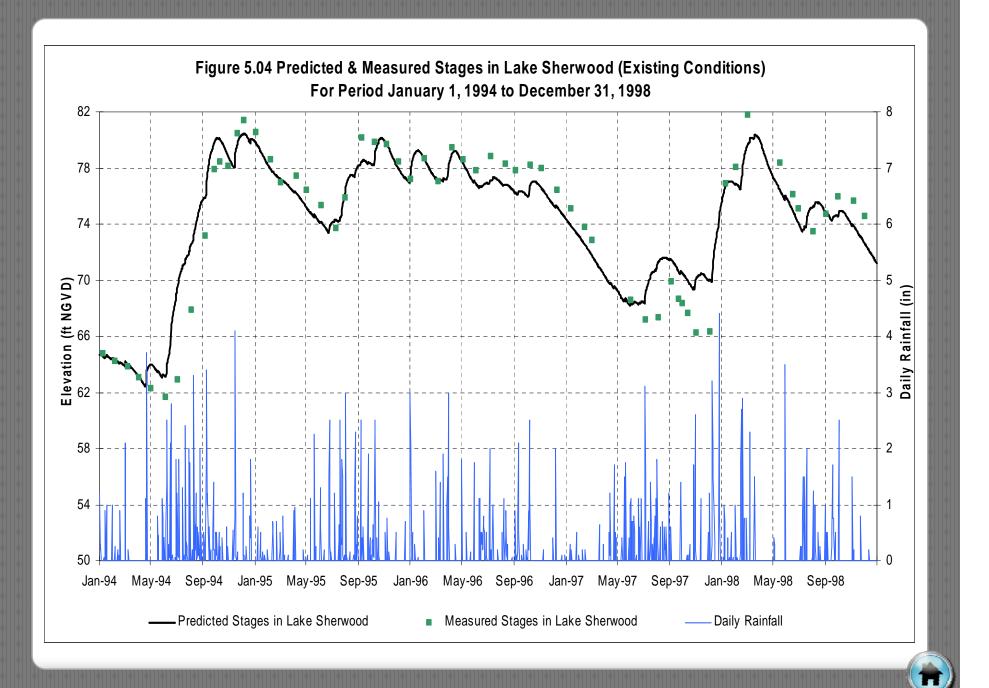
Measured and Predicted Lake Levels – Clermont Chain



Example: Lake Sherwood Closed Basin Lake with Drainage Well



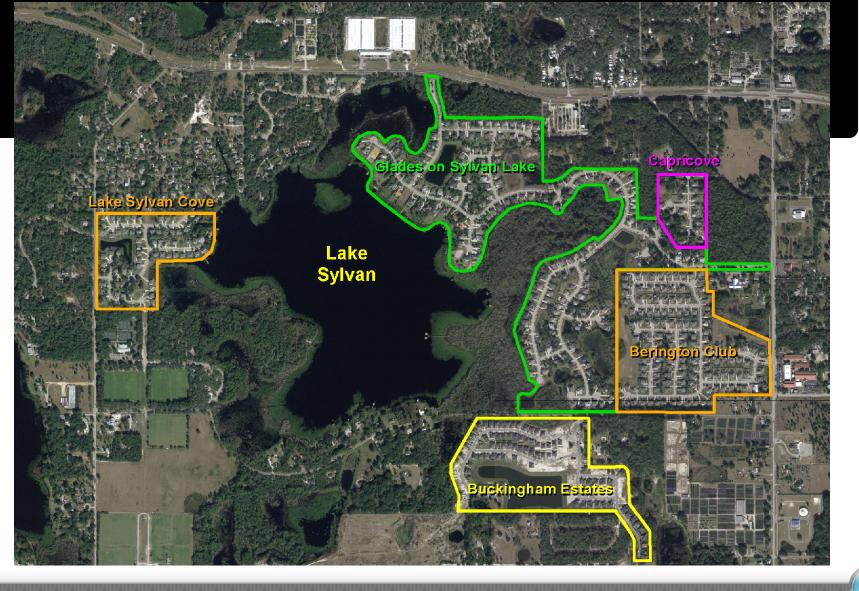




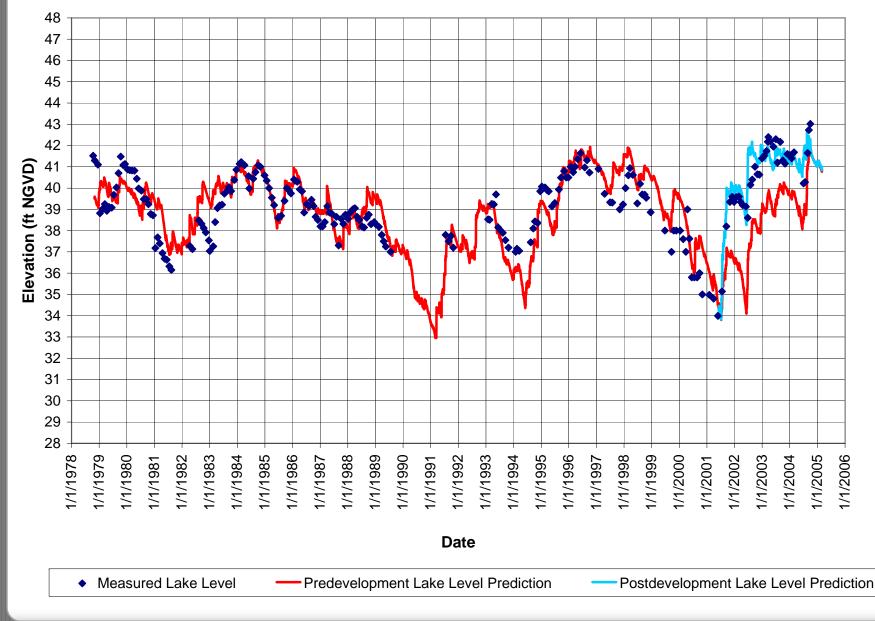
Lake Sylvan - Predevelopment

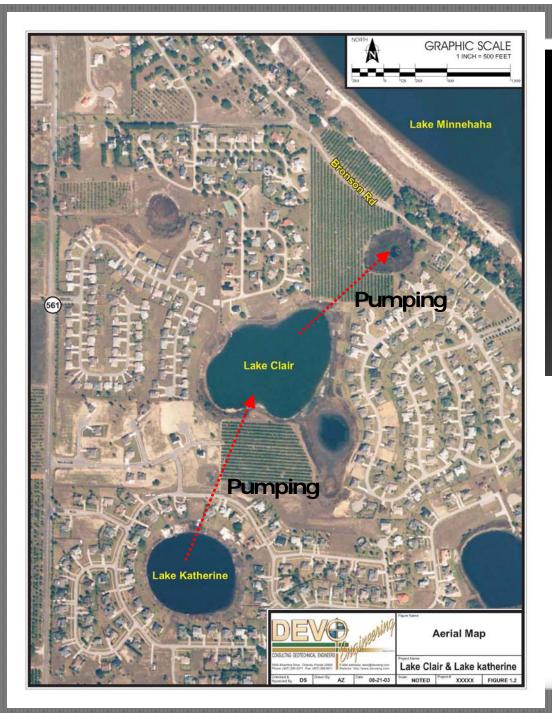


Lake Sylvan - Postdevelopment



Measured and Predicted Lake Levels – Lake Sylvan



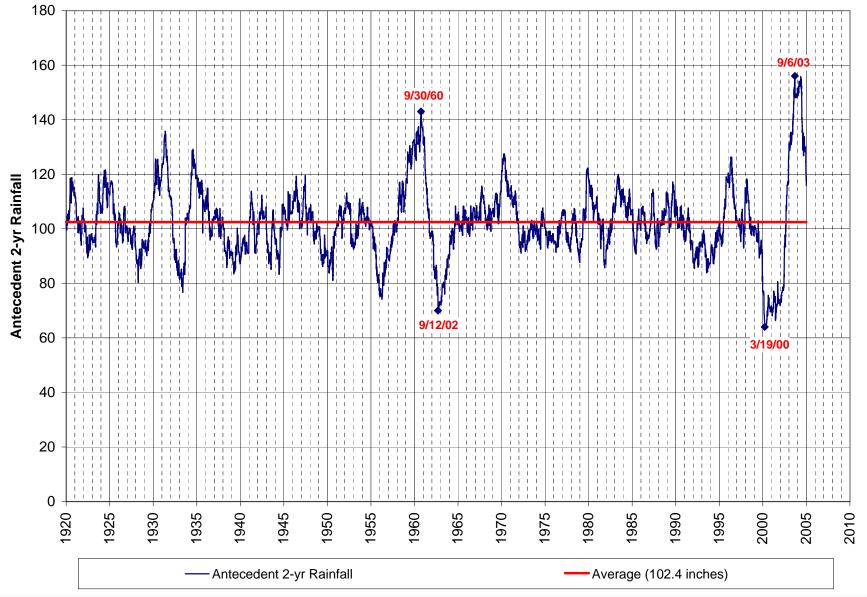


Example:

Lake Katherine / Lake Clair

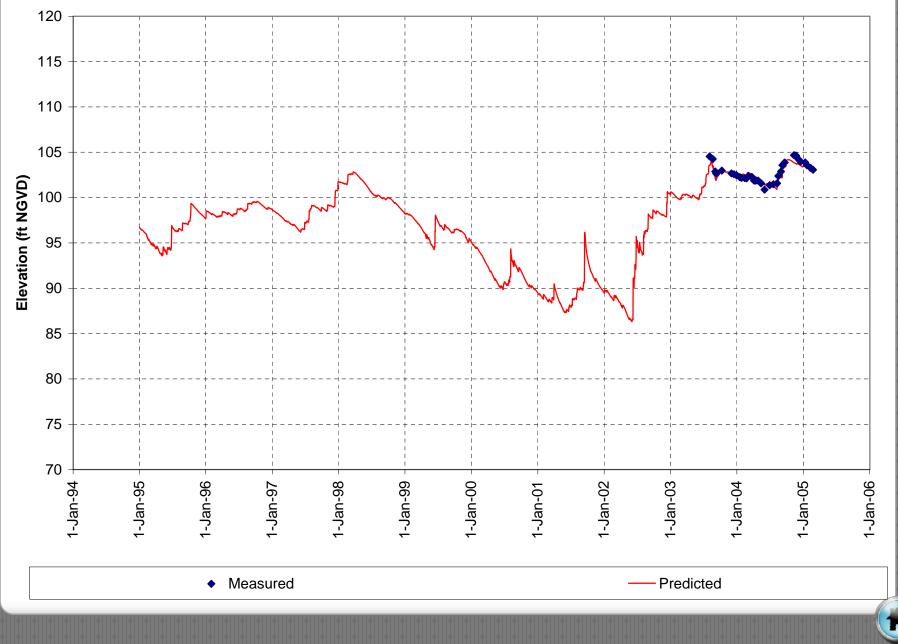
Closed basin flooding with emergency pumping in July/August 2003

2-Year Antecedent Rainfall (Clermont)



1

Model Results for Lake Katherine



Model Results for Lake Clair

